

To make the discussion more concrete, we shall concentrate on the spring-mass incarnation of a harmonic oscillator, but similar considerations hold for other types of oscillators.

We have seen a RLC circuit, a cork in a pond. There are many more.

Recall that the equation of motion is

$$m \frac{d^2y}{dt^2} + d \frac{dy}{dt} + k y = F(t)$$

mass of object attached to spring      damping constant      spring constant      driving force

Dividing by  $m$  and rewriting slightly,

$$\frac{d^2y}{dt^2} + 2 \left( \frac{d}{2m} \right) \frac{dy}{dt} + \left( \frac{k}{m} \right) y = \frac{F}{m}$$

Introduce the notation

$$\frac{d}{2m} = \gamma,$$

$\frac{k}{m} = \omega_0^2$ , "  $\omega_0$ " is called the natural frequency of the system.

$\frac{F}{m} = f$ . It is the frequency the system would oscillate with without damping and forcing.

Indeed,  $\frac{d^2y}{dt^2} + \omega_0^2 y = 0$  has characteristic polynomial  $\chi(z) = z^2 + \omega_0^2 = (z - i\omega_0)(z + i\omega_0)$ .  
Hence solutions  $c_1 \cos(\omega_0 t) + c_2 \sin(\omega_0 t) = A \cos(\omega_0 t + \varphi)$

↑  
frequency  
of oscillation

With this notation, the equation becomes

$$\frac{d^2y}{dt^2} + 2\gamma \frac{dy}{dt} + \omega_0^2 y = f.$$

The associated homogeneous equation is

$$\frac{d^2y}{dt^2} + 2\gamma \frac{dy}{dt} + \omega_0^2 y = 0.$$

This has characteristic polynomial

$$\chi(z) = z^2 + 2\gamma z + \omega_0^2.$$

As before, the roots of the characteristic polynomial may be found using the quadratic formula:

$$\frac{-2\gamma \pm \sqrt{4\gamma^2 - 4\omega_0^2}}{2} = -\gamma \pm \sqrt{\gamma^2 - \omega_0^2}.$$

Suppose that  $\gamma^2 - \omega_0^2 < 0$ , so that the roots are complex.

A basis of solutions is then given by

$$\left\{ e^{-\gamma t} \cos(\sqrt{\omega_0^2 - \gamma^2} t), e^{-\gamma t} \sin(\sqrt{\omega_0^2 - \gamma^2} t) \right\}.$$

A solution

$$c_1 e^{-\gamma t} \cos(\sqrt{\omega_0^2 - \gamma^2} t) + c_2 e^{-\gamma t} \sin(\sqrt{\omega_0^2 - \gamma^2} t)$$

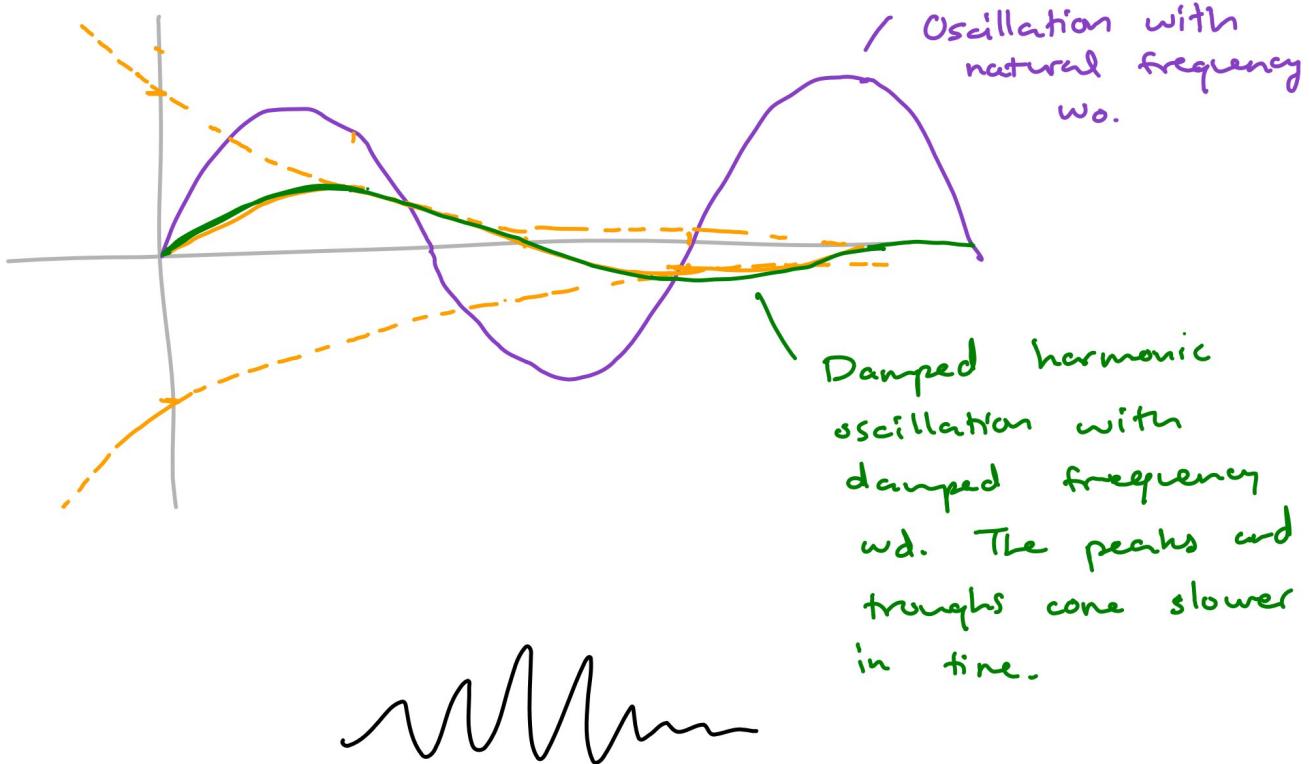
in the span of the basis may be written in phase-amplitude form as

$$A e^{-\gamma t} \cos(\sqrt{\omega_0^2 - \gamma^2} t + \alpha), \quad A \geq 0, \quad \alpha \in (-\pi, \pi].$$

We see that the frequency of the underdamped oscillation is  $\sqrt{\omega_0^2 - \gamma^2} < \omega_0$ .

It becomes equal to the natural frequency  $\omega_0$  when the damping  $\gamma$  is zero, as we may have expected.

We denote  $\sqrt{\omega_0^2 - \gamma^2}$  by  $\omega_d$ , and call it the damped frequency.



(Relatively unimportant) aside: how to estimate how much smaller  $\omega_d$  is than  $\omega_0$ ?

$$\frac{\omega_d}{\omega_0} = \sqrt{\frac{\omega_0^2 - \gamma^2}{\omega_0^2}} = \sqrt{\frac{\omega_0^2 - \gamma^2}{\omega_0^2}} = \sqrt{1 - \frac{\gamma^2}{\omega_0^2}}$$

= Expand in Taylor series.

A way of finding the Taylor expansion of  $(1+x)^\alpha$ ,  $\alpha \in \mathbb{R}$ , without computing derivatives makes use of:

Def. For  $\alpha \in \mathbb{R}$  and  $k \in \mathbb{N}$ , the generalized binomial coefficient is defined to be

$$\binom{\alpha}{k} := \frac{\alpha(\alpha-1)\cdots(\alpha-k+1)}{k!}$$

Note when  $\alpha \in \mathbb{Z}$ , this is the same as the binomial coefficient defined previously:

$$\begin{aligned}\binom{n}{k} &= \frac{n!}{k!(n-k)!} = \frac{1}{k!} \left( \frac{n(n-1)\cdots(n-k+1)(n-k)\cdots 2 \cdot 1}{(n-k)(n-k-1)\cdots 2 \cdot 1} \right) \\ &= \frac{n(n-1)\cdots(n-k+1)}{k!}\end{aligned}$$

Examples:

$$\binom{\frac{1}{2}}{0} = 1 \quad (\text{by convention})$$

$$\binom{\frac{1}{2}}{1} = \frac{\frac{1}{2}}{1!} = \frac{1}{2}$$

$$\binom{\frac{1}{2}}{2} = \frac{\frac{1}{2}(\frac{1}{2}-1)}{2!} = \frac{\frac{1}{2}(-\frac{1}{2})}{2} = -\frac{1}{8}$$

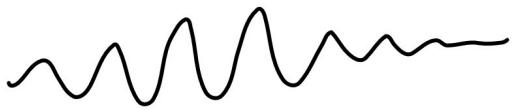
$$\binom{\frac{1}{2}}{3} = \frac{\frac{1}{2}(\frac{1}{2}-1)(\frac{1}{2}-2)}{3!} = \frac{\frac{1}{2}(-\frac{1}{2})(-\frac{3}{2})}{6} = \frac{3}{48} = \frac{1}{16}$$

We have Newton's binomial series:

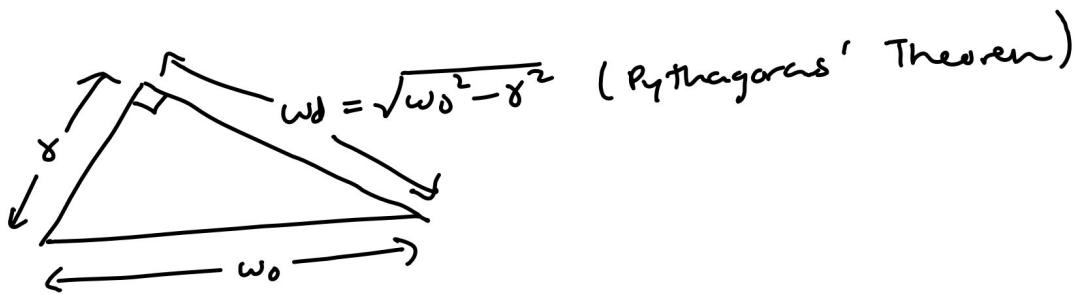
$$(1+x)^\alpha = \sum_{k=0}^{\infty} \binom{\alpha}{k} x^k.$$

$$\text{Therefore, } (1+x)^{\frac{1}{2}} = \sum_{k=0}^{\infty} \binom{\frac{1}{2}}{k} x^k = 1 + \frac{1}{2}x - \frac{1}{8}x^2 + \frac{1}{16}x^3 + \dots$$

$$\text{Finally, } \sqrt{1 - \frac{\gamma^2}{\omega_0^2}} = \left(1 - \frac{\gamma^2}{\omega_0^2}\right)^{1/2} \approx 1 - \frac{1}{2} \frac{\gamma^2}{\omega_0^2} - \frac{1}{8} \frac{\gamma^4}{\omega_0^4} - \frac{1}{16} \frac{\gamma^6}{\omega_0^6}$$



The relationship between the natural frequency  $\omega_0$ , the damped frequency  $\omega_d$  and  $\gamma$  may be displayed on a right triangle:



Now that we understand a bit more about the underdamped oscillations, including the damped frequency  $\omega_d$ , let's study the following question:

What is the resulting motion if the damped spring-mass system is driven by a motor exerting the periodic force

$$F(t) = m F_0 \cos(\omega t), \quad \text{with driving frequency } \omega?$$

( $F_0$  is a constant)

The equation of motion is

$$\frac{d^2y}{dt^2} + 2\gamma \frac{dy}{dt} + \omega_0^2 y = F_0 \cos(\omega t).$$

Let's use the method of undetermined coefficients to find a particular solution.

For  $F_0 \cos(\omega t)$ , a possible annihilator is

$$\left( \frac{d}{dt} - i\omega \right) \left( \frac{d}{dt} + i\omega \right).$$

Applying this to both sides of (\*), we get the homogeneous linear equation

$$\left( \frac{d}{dt} - i\omega \right) \left( \frac{d}{dt} + i\omega \right) \left( \frac{d}{dt} - (-\gamma + \sqrt{\gamma^2 - \omega_0^2}) \right) \left( \frac{d}{dt} - (-\gamma - \sqrt{\gamma^2 - \omega_0^2}) \right) = 0$$

Because the roots of  $x(z)$  have a real part (equal to  $-\gamma$ , which we are assuming is not zero),

$x(\frac{d}{dt})$  has no shared factors with the annihilator. Therefore, discarding solutions to the associated homogeneous equation for now, we should look for  $\phi_p$  in the span of

$$\{ \cos(\omega t), \sin(\omega t) \}$$

Basis elements corresponding to the annihilator.

$$\varphi_p(t) = c_1 \cos(\omega t) + c_2 \sin(\omega t)$$

$$\varphi_p'(t) = -\omega c_1 \sin(\omega t) + \omega c_2 \cos(\omega t)$$

$$\varphi_p''(t) = -\omega^2 c_1 \cos(\omega t) - \omega^2 c_2 \sin(\omega t)$$

Thus,

$$\begin{aligned} \varphi_p'' + 2\gamma\varphi_p' + \omega_0^2\varphi_p \\ = (-\omega^2 c_1 + 2\gamma\omega c_2 + \omega_0^2 c_1) \cos(\omega t) \\ + (-\omega^2 c_2 - 2\gamma\omega c_1 + \omega_0^2 c_2) \sin(\omega t) \end{aligned}$$

For  $\varphi_p$  to be a particular solution, this should equal  $F_0 \cos(\omega t) (+ 0 \cdot \sin(\omega t))$ .

Matching coefficients, we obtain the system of equations

$$\left. \begin{array}{l} (1) \quad (\omega_0^2 - \omega^2) c_1 + 2\gamma\omega c_2 = F_0 \\ (2) \quad (\omega_0^2 - \omega^2) c_2 - 2\gamma\omega c_1 = 0 \end{array} \right\}$$

From (2),  $c_1 = \frac{\omega_0^2 - \omega^2}{2\gamma\omega} c_2$ . Into (1),

$$\left( \frac{(\omega_0^2 - \omega^2)^2}{2\gamma\omega} + 2\gamma\omega \right) c_2 = F_0$$

$$S_0 \quad \left( \frac{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2}{2\gamma\omega} \right) c_2 = F_0$$

$$c_2 = \left( \frac{2\gamma\omega}{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2} \right) F_0$$

$$c_1 = \left( \frac{\omega_0^2 - \omega^2}{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2} \right) F_0$$

are the  
solutions.

We would like to write

$$c_1 \cos(\omega t) + c_2 \sin(\omega t) = A \cos(\omega t + \phi)$$

for some  $A$  and  $\phi$ . Recall from the homework that

$$\begin{aligned} A \cos(\omega t + \phi) &= A (\cos(\omega t) \cos(\phi) - \sin(\omega t) \sin(\phi)) \\ &= (A \cos(\phi)) \cos(\omega t) + (-A \sin(\phi)) \sin(\omega t) \end{aligned}$$

$$\begin{aligned} c_1 &= A \cos(\phi) && \left( \text{This uses uniqueness of a} \right. \\ c_2 &= -A \sin(\phi) && \left. \text{representation of a vector in} \right. \\ &&& \left. \text{terms of basis elements} \right) \end{aligned}$$

$$S_0 \quad c_1^2 + c_2^2 = A^2 (\cos^2(\phi) + \sin^2(\phi)) = A^2.$$

$$A = \sqrt{c_1^2 + c_2^2}$$

$$\text{and } -\frac{c_2}{c_1} = \tan(\phi).$$

We compute, with the previously found  $c_1$  and  $c_2$ , that

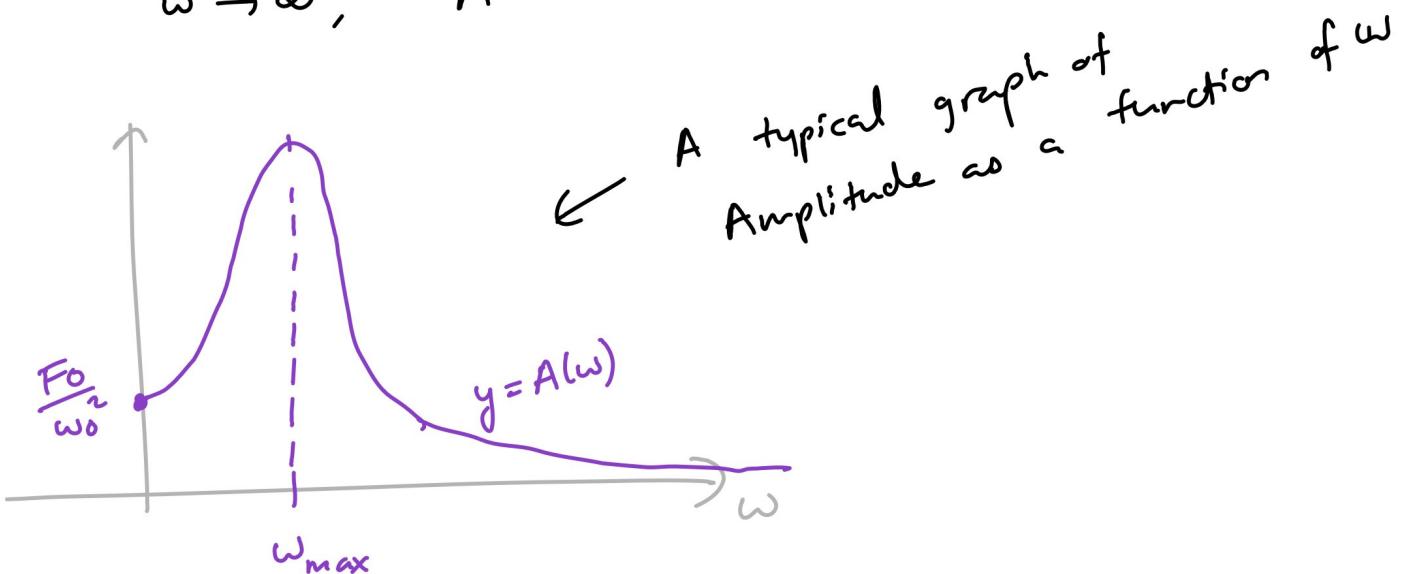
$$\begin{aligned}\frac{1}{F_0^2}(c_1^2 + c_2^2) &= \left( \frac{(\omega_0^2 - \omega^2)}{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2} \right)^2 + \left( \frac{2\gamma\omega}{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2} \right)^2 \\ &= \frac{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2}{[(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2]^2} = \frac{1}{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2}\end{aligned}$$

So that the amplitude of the particular solution  $\varphi_p$  is

$$A = \sqrt{c_1^2 + c_2^2} = \frac{F_0}{\sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2}}$$

$$\text{As } \omega \rightarrow 0, \quad A \rightarrow \frac{F_0}{\omega_0^2}$$

$$\omega \rightarrow \infty, \quad A \rightarrow 0$$



is called the resonant frequency

$$\omega_{\max} = \sqrt{\omega_0^2 - 2\gamma^2} \quad (\text{as you will check in homework!})$$

$$\frac{C_2}{C_1} = \frac{\frac{2\gamma\omega}{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2}}{\frac{(\omega_0^2 - \omega^2)}{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2}} = \frac{2\gamma\omega}{\omega_0^2 - \omega^2}$$

$$\tan \phi = - \frac{C_2}{C_1} = \frac{2\gamma\omega}{\omega^2 - \omega_0^2}$$

As  $\omega \rightarrow 0$ ,  $\tan \phi \rightarrow 0$ , so  $\phi \rightarrow 0$   
 The driving force and the motion  
 are in phase

$\omega \rightarrow \omega_0$ ,  $\tan \phi \rightarrow \infty$ , so  $\phi \rightarrow -\frac{\pi}{2}$   
 The driving force and the motion  
 are  $\frac{\pi}{2}$  out of phase.

$\omega \rightarrow \infty$ ,  $\tan \phi \rightarrow 0$  again, this time  $\phi \rightarrow -\pi$ .

